

Consequently, all the derivatives of  $F_{im}$  must vanish, so that it is a constant orthogonal matrix, *i.e.* a rotation (excluding reflections).

**10.16**

$$\{u_{ij}\} = \frac{1}{2} \begin{pmatrix} 34 & -9 & 0 \\ -9 & 73 & 17 \\ 0 & 17 & 29 \end{pmatrix}$$

**10.17** Use that the determinant of a product of matrices is the product of the determinant to get  $\det \delta_{ij} + 2u_{ij} = \det |\delta_{ij} + \nabla_j u_i|^2$ .

## 11 Elasticity

**11.1** Expanding to first order in  $r - a$ , we have for  $r$  close to  $a$

$$f(r) = f(a) + (r - a)f'(a) .$$

With  $\Delta F = f(r) - f(a)$ ,  $\Delta L = r - a$ , and  $k = f'(a)$  this is Hooke's law.

**11.2** b)  $\omega^2 = 4 \sin^2 \frac{k}{2}$ .

**11.6** The absolute minimum of the coefficient of the first term happens for  $\alpha = 1/3$ .

**11.7**

(a) Follows from the symmetry of  $\sigma_{ij}$  and  $u_{ij}$ .

(b) In order for  $\delta u_{ij} \Delta \sigma_{ij} = \delta u_{ij} \lambda_{ijkl} u_{kl}$  to become a total differential  $\delta(\frac{1}{2} \lambda_{ijkl} u_{ij} u_{kl})$ , the  $9 \times 9$ -matrix  $\lambda_{(ij)(kl)}$  must be symmetric.

## 12 Solids at rest

**12.4** We use that  $u_{zz}$  is linear in  $x$  and  $y$ , of the form

$$u_{zz} = \nabla_z u_z = \alpha - \beta_x x - \beta_y y$$

and consequently

$$u_z = a_z - \phi_y x + \phi_x y + \alpha z - \beta_x x z - \beta_y y z$$

where the coefficients are all constants. Using this result, we find  $\nabla_x u_x = \nabla_y u_y = -\nu(\alpha - \beta_x x - \beta_y y)$ . Integrating and demanding that  $u_{xy} = u_{xz} = u_{zy} = 0$ , we obtain the most general form

$$u_x = a_x - \phi_z y + \phi_y z - \alpha \nu x + \frac{1}{2} \beta_x (z^2 - \nu(x^2 - y^2)) - \beta_y \nu x y , \quad (12-A1a)$$

$$u_y = a_y + \phi_z x - \phi_x z - \alpha \nu y + \frac{1}{2} \beta_y (z^2 - \nu(y^2 - x^2)) - \beta_x \nu x y , \quad (12-A1b)$$

$$u_z = a_z - \phi_y x + \phi_x y + \alpha z - \beta_x x z - \beta_y y z . \quad (12-A1c)$$

Here  $(a_x, a_y, a_z)$  represents simple translations of the body, and  $(\phi_x, \phi_y, \phi_z)$  simple rotations around the coordinate axes. The coefficient  $\alpha$  corresponds to a uniform stretching, and only  $(\beta_x, \beta_y)$  represents bending into the coordinate directions.

**12.5** Same general solution as for the pressurized tube but with  $a$  and  $b$  interchanged

$$A = -\frac{1}{2(\lambda + \mu)} \frac{b^2}{b^2 - a^2} P = -(1 + \sigma)(1 - 2\sigma) \frac{b^2}{b^2 - a^2} \frac{P}{E},$$

$$B = -\frac{1}{2\mu} \frac{a^2 b^2}{b^2 - a^2} P = -(1 + \sigma) \frac{a^2 b^2}{b^2 - a^2} \frac{P}{E}.$$

The rest is straightforward.

**12.6** a) The centrifugal force density is radial and given by  $f_r = \rho_0 \Omega^2 r$ . b) The general solution to (12-46) is

$$u_r = Ar + \frac{B}{r} - \frac{1}{8} \frac{\rho_0 \Omega^2}{\lambda + 2\mu} r^3. \quad (12-A2)$$

where  $A$  and  $B$  are integration constants. Use that  $u_r$  must be finite for  $r = 0$  and  $\sigma_{rr} = 0$  for  $r = a$ . The final solution becomes

$$u_r = \frac{1}{8} \frac{\rho_0 \Omega^2 a^2}{\lambda + 2\mu} r \left( 3 - 2\nu - \frac{r^2}{a^2} \right), \quad (12-A3)$$

c) The strains are

$$u_{rr} = \frac{1}{8} \frac{\rho_0 \Omega^2 a^2}{\lambda + 2\mu} \left( 3 - 2\nu - 3 \frac{r^2}{a^2} \right), \quad u_{\phi\phi} = \frac{1}{8} \frac{\rho_0 \Omega^2 a^2}{\lambda + 2\mu} \left( 3 - 2\nu - \frac{r^2}{a^2} \right). \quad (12-A4)$$

The radial strain is positive for  $r = 0$ , vanishes for  $r = a\sqrt{1 - 2\nu/3}$ , and is negative for  $r = a$ . d) Breakdown happens for  $r = 0$  where the extension and tension is maximal.

**12.9** The total force is

$$\mathcal{F}_z = \int_A \sigma_{zz} ds_z = -\frac{E}{R} I_x. \quad (12-A5)$$

If the area  $A$  is symmetric under reflection in the  $y$ -axis, then  $I_x = 0$ .

**12.10** Letting  $x \rightarrow x + \alpha$  in (12-20), we get

$$u_x = \frac{\nu}{2R} \alpha^2 + \frac{\nu}{R} \alpha x + \frac{1}{2R} (z^2 + \nu(x^2 - y^2)),$$

$$u_y = \frac{\nu}{R} \alpha y + \frac{\nu}{R} xy,$$

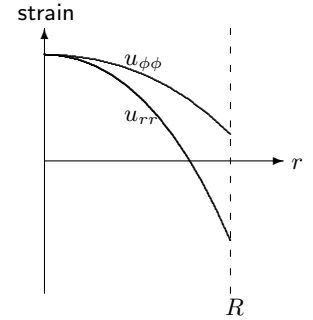
$$u_z = -\frac{1}{R} \alpha z - \frac{1}{R} xz.$$

The first column represents a simple translation and the second a uniform stretching of the form (11-24).

## 13 Vibrations

**13.1** For an arbitrary vector field we first find a solution  $\psi$  to the equation

$$\nabla^2 \psi = \nabla \cdot \mathbf{u} \quad (13-A1)$$



Sketch of strains in the massive rotating cylinder.