

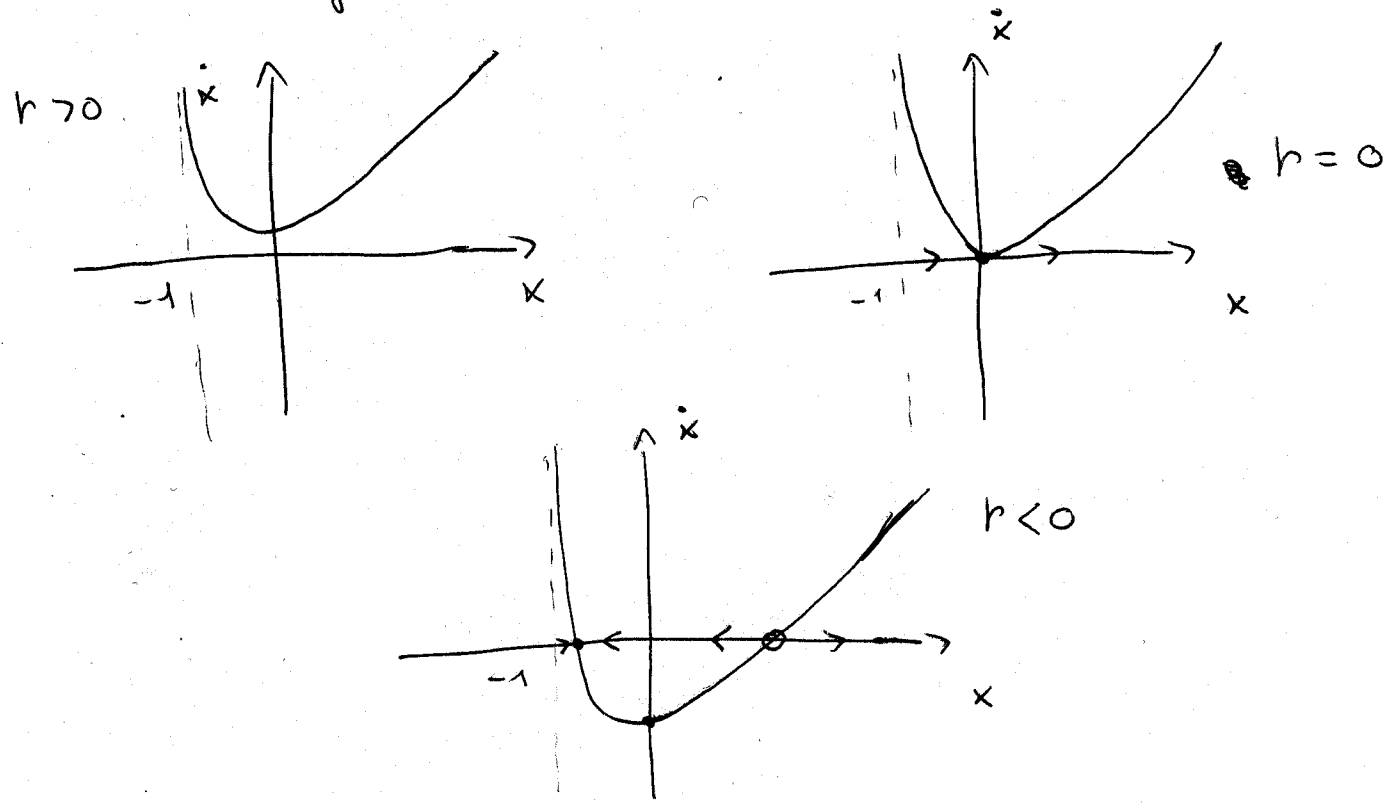
3.1.3

$$\dot{x} = r + x - \ln(1+x) \equiv f(x)$$

$f(x) \rightarrow +\infty$  when  $x \rightarrow \pm\infty$ ,  $f(x) \rightarrow +\infty$  when  $x \rightarrow -1$

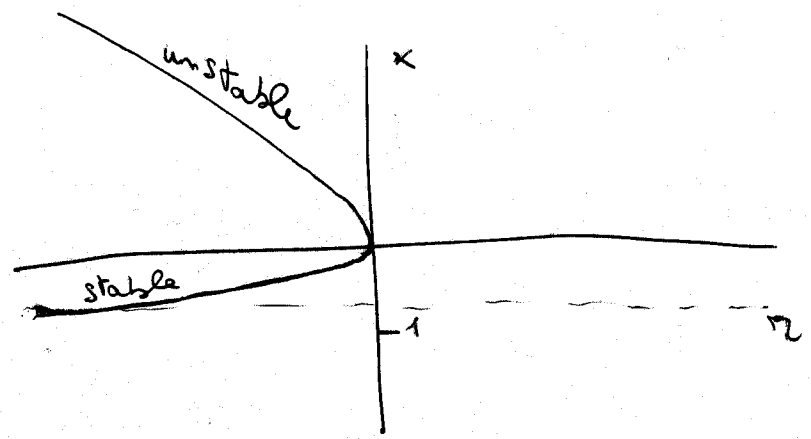
$$f'(x) = 1 - \frac{1}{1+x} = 0 \Leftrightarrow x = 0, \text{ so that the}$$

vector field looks like this



the bifurcation diagram is given by the ~~curve~~ curve

$$r + x - \ln(1+x) = 0$$



a pair of fixed points (one stable and one unstable) is created as  $r$  turns negative, ~~and~~ that is we are in <sup>the</sup> presence of a tangent (a saddle-node) bifurcation.

3.2.6

$$a) \quad \dot{x} = R\bar{x} - \bar{x}^2 + O(\bar{x}^4) \quad (1)$$

$$\text{if } \bar{x} = x + cx^3 + O(x^4) \quad (2)$$

plug (1) ~~into~~ into (2) and get

$$\bar{x} = \bar{x} + b\bar{x}^3 + c(\bar{x} + b\bar{x}^3)^3 + O(\bar{x}^4)$$

$\Leftrightarrow$

$$0 = b\bar{x}^3 + c\bar{x}^3 + O(\bar{x}^4)$$

$$\Rightarrow c = -b + O(\bar{x}^4)$$

$$b) \quad \dot{\bar{x}} = \dot{\bar{x}} + 3b\bar{x}^2\dot{\bar{x}} + O(\bar{x}^4) =$$

$$= R\bar{x} - \bar{x}^2 + a\bar{x}^3 + 3b\bar{x}^2(R\bar{x} - \bar{x}^2 + a\bar{x}^3) + O(\bar{x}^4)$$

$$= R\bar{x} - \bar{x}^2 + (a + 3bR)\bar{x}^3 + O(\bar{x}^4)$$

$$= R \left( x - bx^3 + O(x^4) \right) - \left( x - bx^3 + O(x^4) \right)^2 + (a + 3bR) \left( x - bx^3 + O(x^4) \right)^3 =$$

$$Rx - x^2 + (a + 2bR)x^3 + O(x^4)$$

c) The  $x^3$  term vanishes if  $b = -\frac{a}{2R}$

d)  $R \neq 0$  is necessary for the transformation to ~~make sense~~ <sup>exist</sup> if  $a \neq 0$ .  
~~if~~ If  $a = 0$  ~~and~~ and  $R = 0$ , then there is no need for it.

3.3.1

$$a) \quad H=0 \quad \Rightarrow \quad N = \frac{P}{G_m + f}$$

$$\text{and } \dot{m} = \frac{PG_m}{G_m + f} - km$$

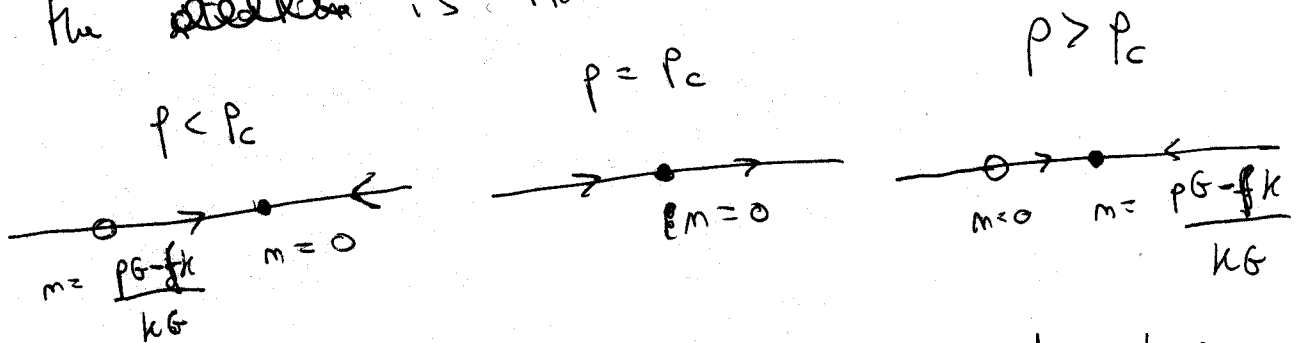
$$b) \quad \dot{m}=0 \quad \text{iff } m=0 \quad \text{or} \quad m = \frac{Pg - fk}{kG}$$

$$\frac{d}{dm} \left[ \frac{PG_m}{G_m + f} - km \right] = \frac{fGp}{(G_m + f)^2} - k, \quad \text{then } m=0$$

the derivative is  $\frac{Gp}{f} - k > 0$  iff  $p > \frac{fk}{G} \equiv p_c$

so that the ~~critical~~ <sup>fixed</sup> point  $m=0$  is unstable above a certain value of the pump strength

c) the ~~critical~~ <sup>bifurcation</sup> is transcritical:



that is our laser turns on when the pump strength is sufficiently high.

d) Rather than a complete analysis, few remarks ~~are~~ are made:  $k$  is proportional to the decay of  $n$ , while  $f$  is proportional to the decay of  $N$ , hence having  $k \ll f$  would help the approximation.

$G$  is proportional to a coupled term ( $nN$ ), hence it is difficult to compare it to the other parameters.

the pump strength is ~~also~~ proportional to ~~the~~ the increase in the number of ~~also~~ excited atoms, but it's either trivially small (no laser) or above a certain threshold (e.g.  $\frac{kf}{G}$ ).

$$\dot{x} = rx - \frac{x}{1+x^2} = 0 \quad \text{iff}$$

$$x(h + rx^2 - 1) = 0, \quad \text{that is}$$

$$x = 0 \quad \text{or} \quad x^* = \pm \sqrt{\frac{1-h}{r}}$$

The last two roots exist only if  $h < 1$ .

$$f'(x) = r - \frac{(1+x^2) - 2x^2}{(1+x^2)^2}, \quad f'(x^*) = r - \frac{2r-1}{r} > 0 \quad \text{if}$$

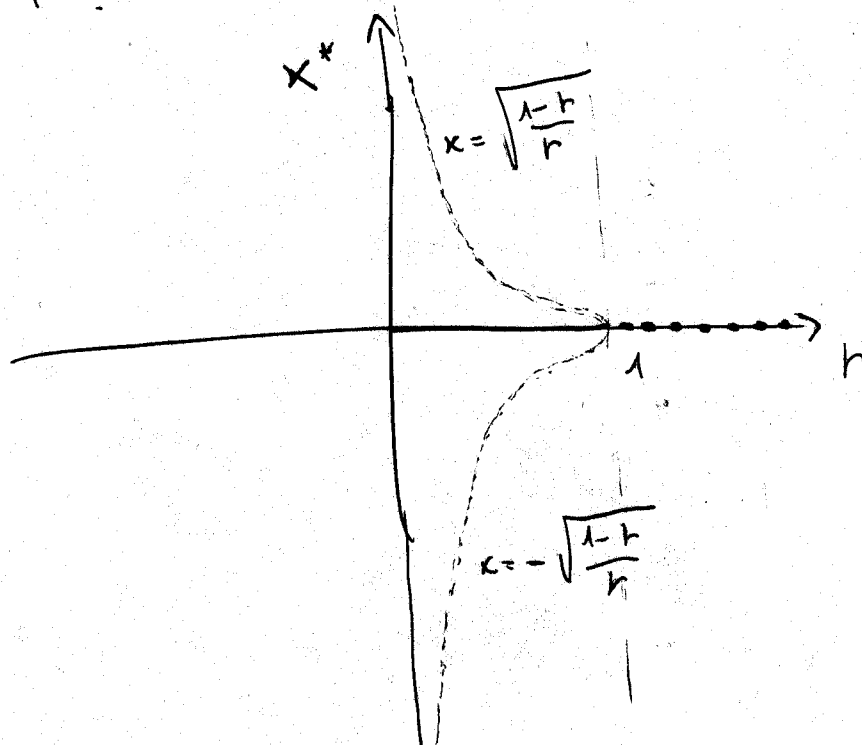
$$\left(\frac{1}{r}\right)^2$$

$$1-h > 0 \Leftrightarrow h < 1.$$

On the other hand,  $f'(0) = r-1 > 0 \Leftrightarrow r > 1$ .

Therefore a subcritical pitchfork bifurcation occurs at

$$h = 1:$$



.5.7

$$\dot{N} = rN(1 - N/K), \quad N(0) = N_0$$

a) If  $N$  is measured in representatives of a given species, then  $N_0$  and hence  $K$  are dimensionless. (Alternatively, both could be measured in units of biomass, e.g., kg.)  
Therefore,  $\dot{N}$  has units of  $\text{sec}^{-1}$  and so does  $r$ .

b) Define  $x = N/K$ , so  $\dot{x} = \frac{\dot{N}}{K} = r \frac{N}{K} (1 - \frac{N}{K}) = rx(1-x)$

If we define  $x_0 = N_0/K$ , then  $x(0) = N(0)/K = N_0/K = x_0$ .

Finally, if we rescale time:  $\tau = rt$ , then

$$\frac{dx}{d\tau} = \frac{dx}{dt} \frac{dt}{d\tau} = \frac{1}{r} r x(1-x) = x(1-x)$$

c) Alternatively, we can choose  $u = N/N_0$ , so  $u(0) = \frac{N(0)}{N_0} = 1$

$$\text{and } \dot{u} = r \frac{N}{N_0} (1 - \frac{N}{N_0} \frac{N_0}{K}) = ru(1 - \frac{N_0}{K} u)$$

Defining  $\tau = rt$  as before and  $k' = \frac{K}{N_0}$ , we obtain

$$\frac{du}{d\tau} = \frac{1}{r} ru(1 - \frac{1}{k'} u) = u(1 - u/k')$$

d) 1<sup>st</sup> nondimensionalization allows easier interpretation of the results in terms of their dependence on critical conditions, while the second one - dependence on the carrying capacity.